

# 2012 Southeastern Transportation Geotechnical Engineering Conference

## Design and Installation of **Micropile Foundations for a Bridge** in Karst Topography

Prepared by:

**Jim Sheahan** HDR Engineering, Inc.

**Chaz Weaver** VDOT

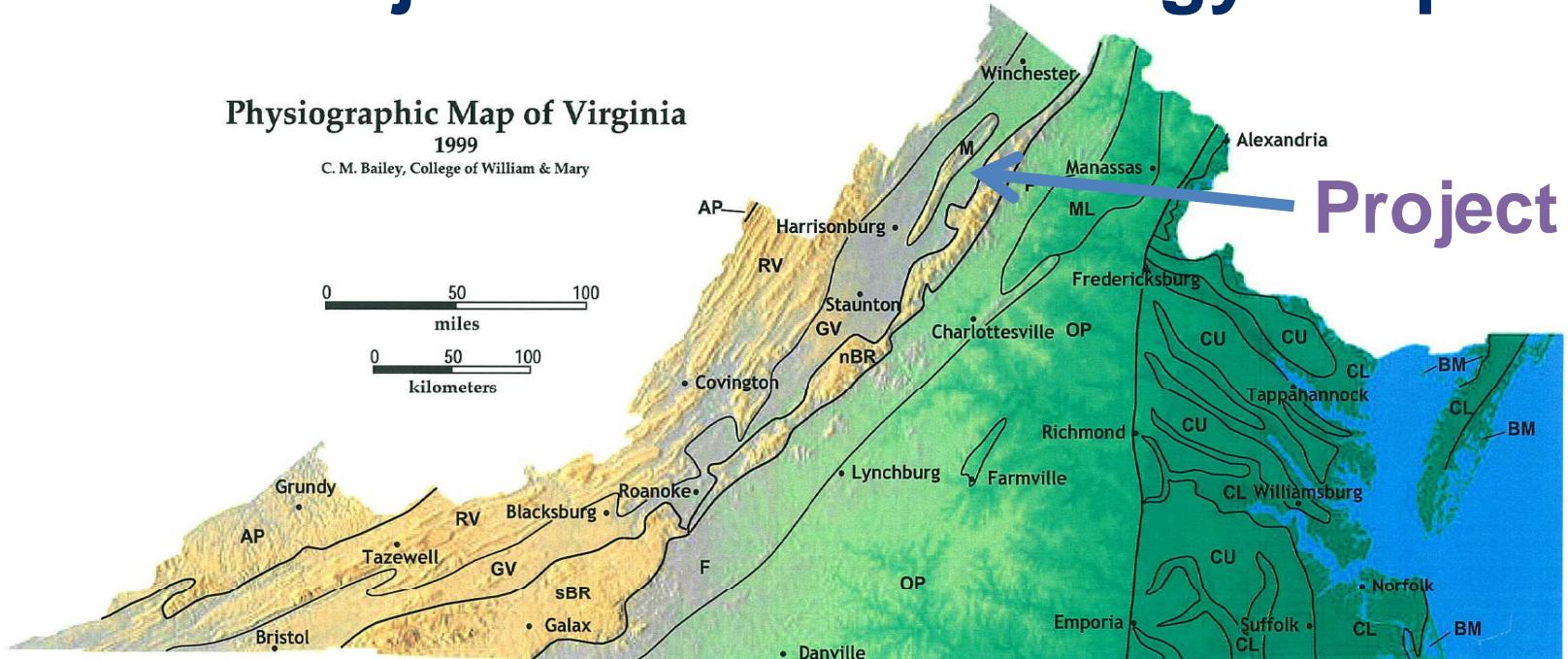
Aaron Zdinak HDR Engineering, Inc.



# Presentation Overview

- Project Location
- Karst
- Geotechnical Explorations
- Foundations Type Selection Considerations
- Design and Construction Considerations
  - Lateral Loading
  - LRFD
  - Installation and Testing
- Construction and Observations
- Load Testing
- Concluding Comments

# Route 340 Project Location/Geology Map



## Appalachian Plateau province

**AP- Rugged, well-dissected landscape with dendritic drainage pattern. Elevation-1000'-3000' with High Knob rising to over 4000'.**

## Valley & Ridge province

**RV- Ridge & Valley**  
subprovince: long linear ridges separated by linear valleys with trellis drainage pattern.  
Elevation- 1000'-4500'.

## Blue Ridge province

**nBR- northern Blue Ridge subprovince:** rugged region with steep slopes narrow ridges, broad mountains, and high relief. Elevation 1500'-4200'

## Piedmont province

**F- Foothills subprovince:**  
region with broad rolling  
hills and moderate slopes.  
Elevation 400'-1000' with  
peaks rising to 1500'-2500'.

## Coastal Plain province

**CU- Upland subprovince:**  
broad upland with low slopes  
and gentle drainage divides.  
Steep slopes develop where  
dissected by stream erosion.  
Elevation- 60'-250'.

**RV- Ridge & Valley**  
**subprovince:** long linear ridges separated by linear valleys with trellis drainage pattern.  
Elevation- 1000'-4500'.

**CV- Great Valley**  
**subprovince:** broad valley with low to moderate slopes underlain by carbonate rocks. Elevation- 500'-1500' north of Roanoke. 1200'-2300' south of Roanoke.

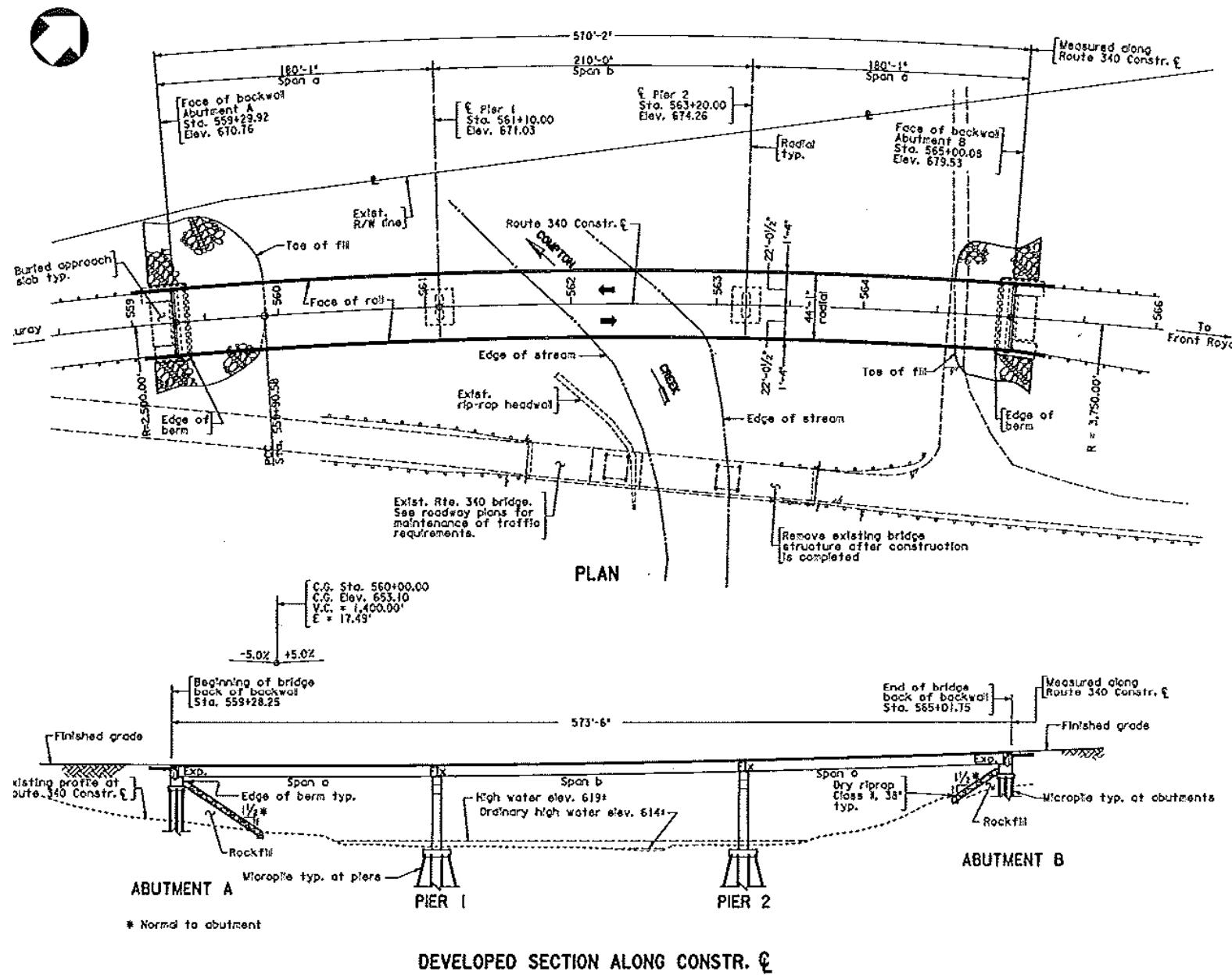
**M- Massanutten Mountain:**  
Series of long linear ridges  
that rise to 3000' above the  
Great Valley

**sBR- southern Blue Ridge subprovince:** broad upland plateau with moderate slopes. Elevation 2400'- 3000' with higher peaks rising above upland, including 5729' Mt. Rogers.

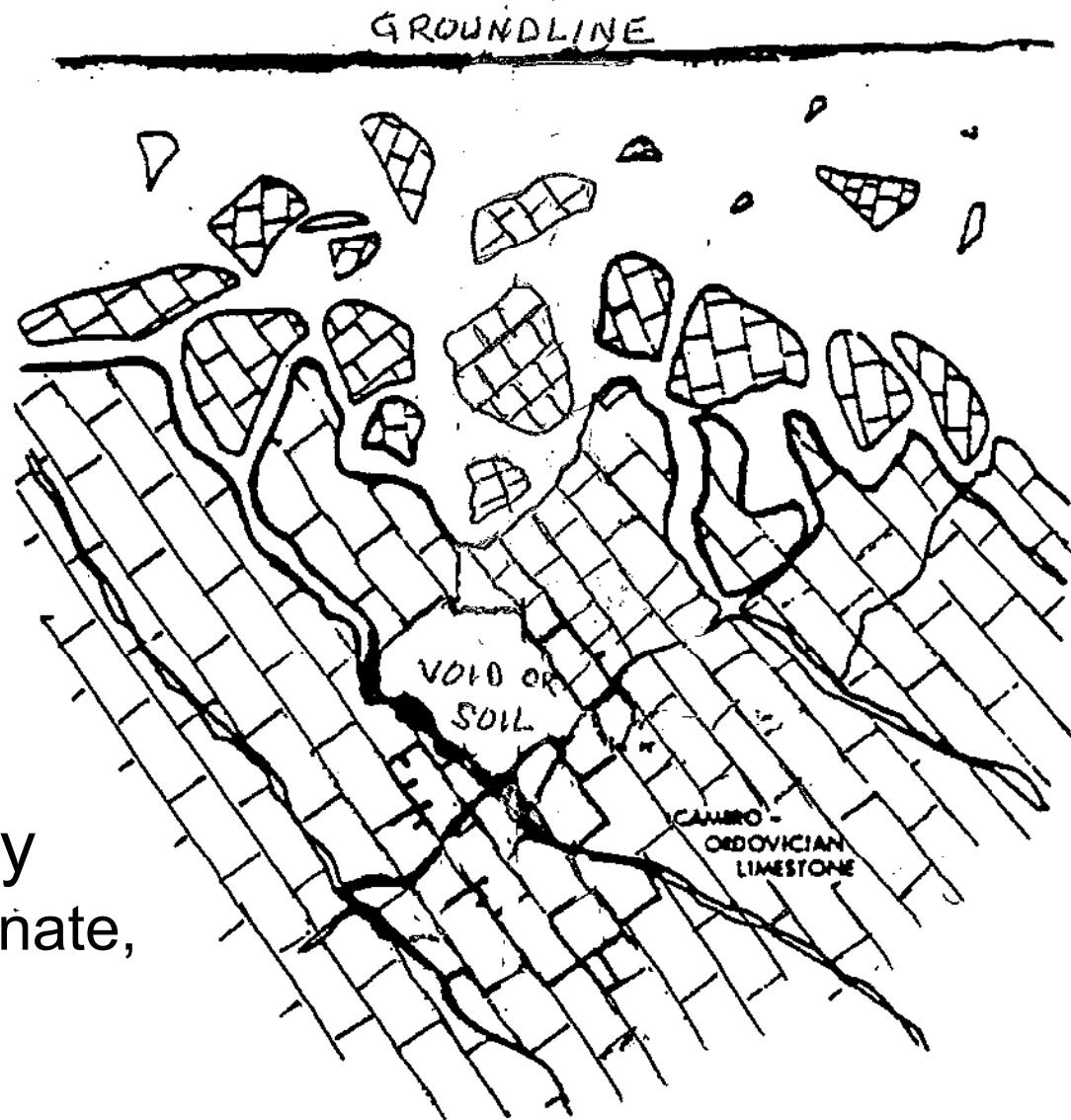
**ML- Mesozoic lowlands subprovince:** region with modest relief and low slopes underlain by Mesozoic sedimentary and igneous rocks. Elevation 300' 400'

**OP- Outer Piedmont**  
subprovince: broad upland  
with low to moderate slopes  
Elevation 600'-1000' in west  
gradually diminishing to  
250'- 300' in east.

**BM- Barrier Islands & Salt Marshes:** low, open areas covered with sediment and vegetation in direct proximity to the Chesapeake Bay and Atlantic Ocean. Elevation 0'-15'.



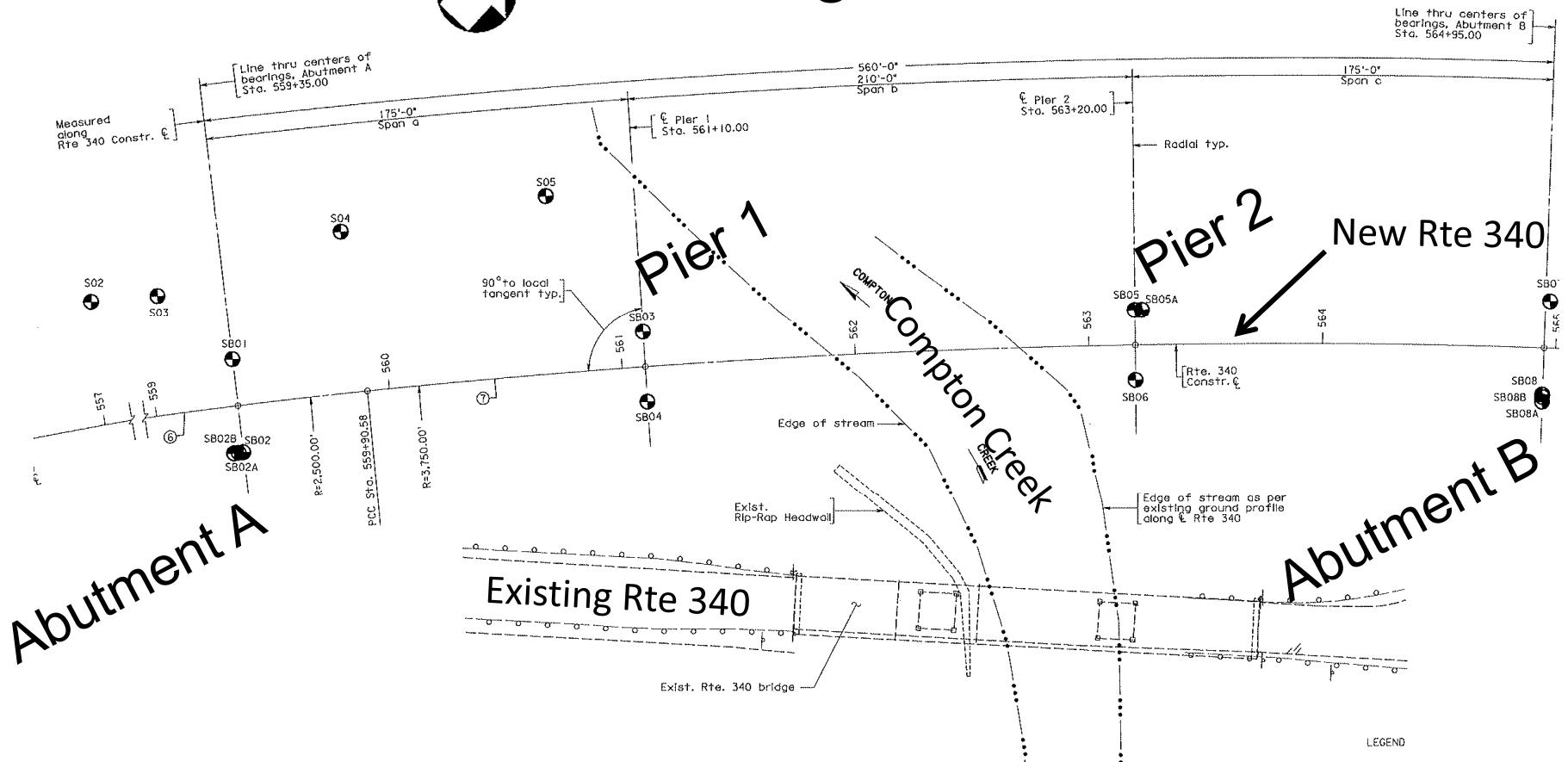
This is Karst !



Project Site Geology

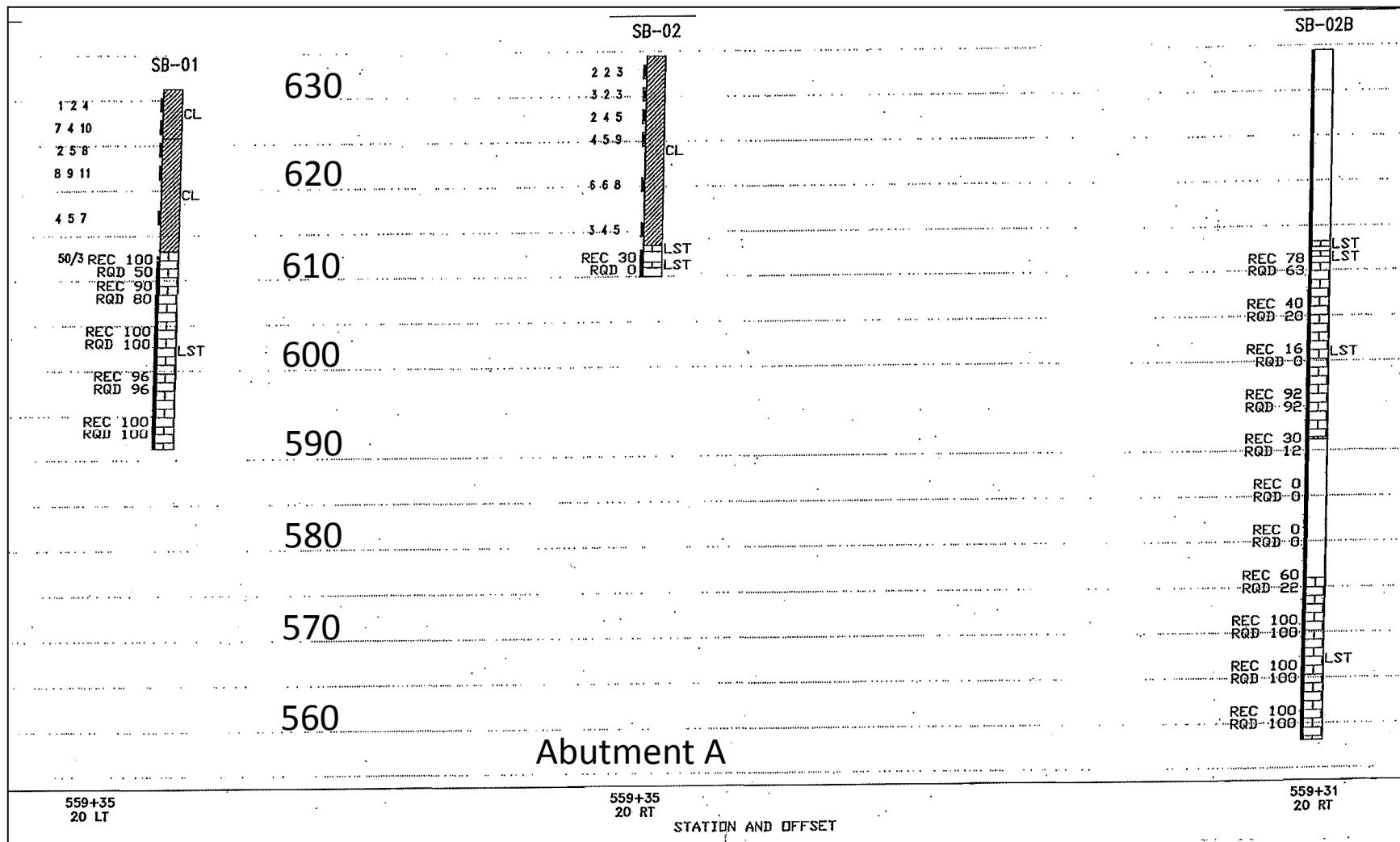
- Highly Soluble, Carbonate, Sedimentary Rocks (Beekmantown Group)

# Boring Location Plan

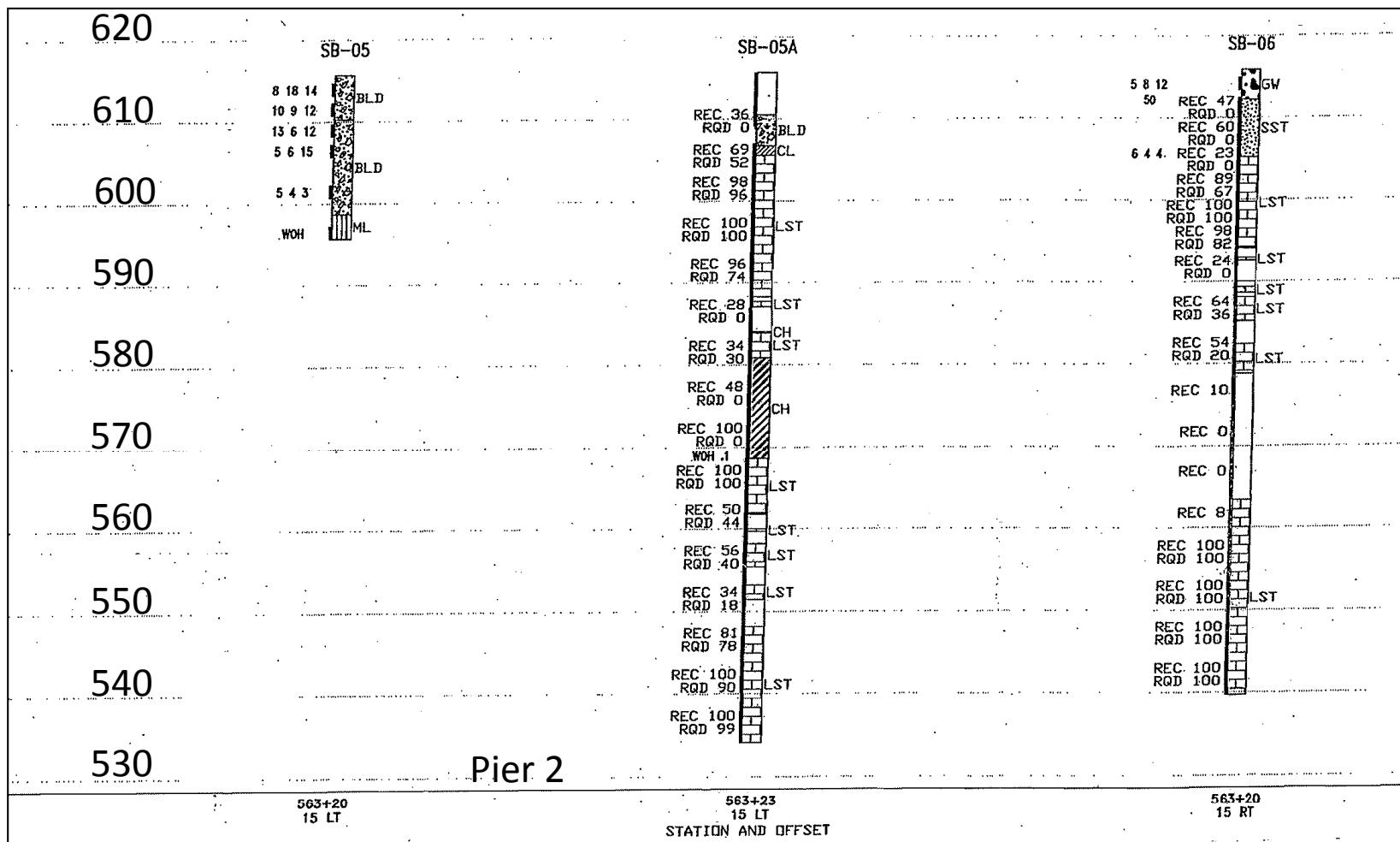


● Boring Location

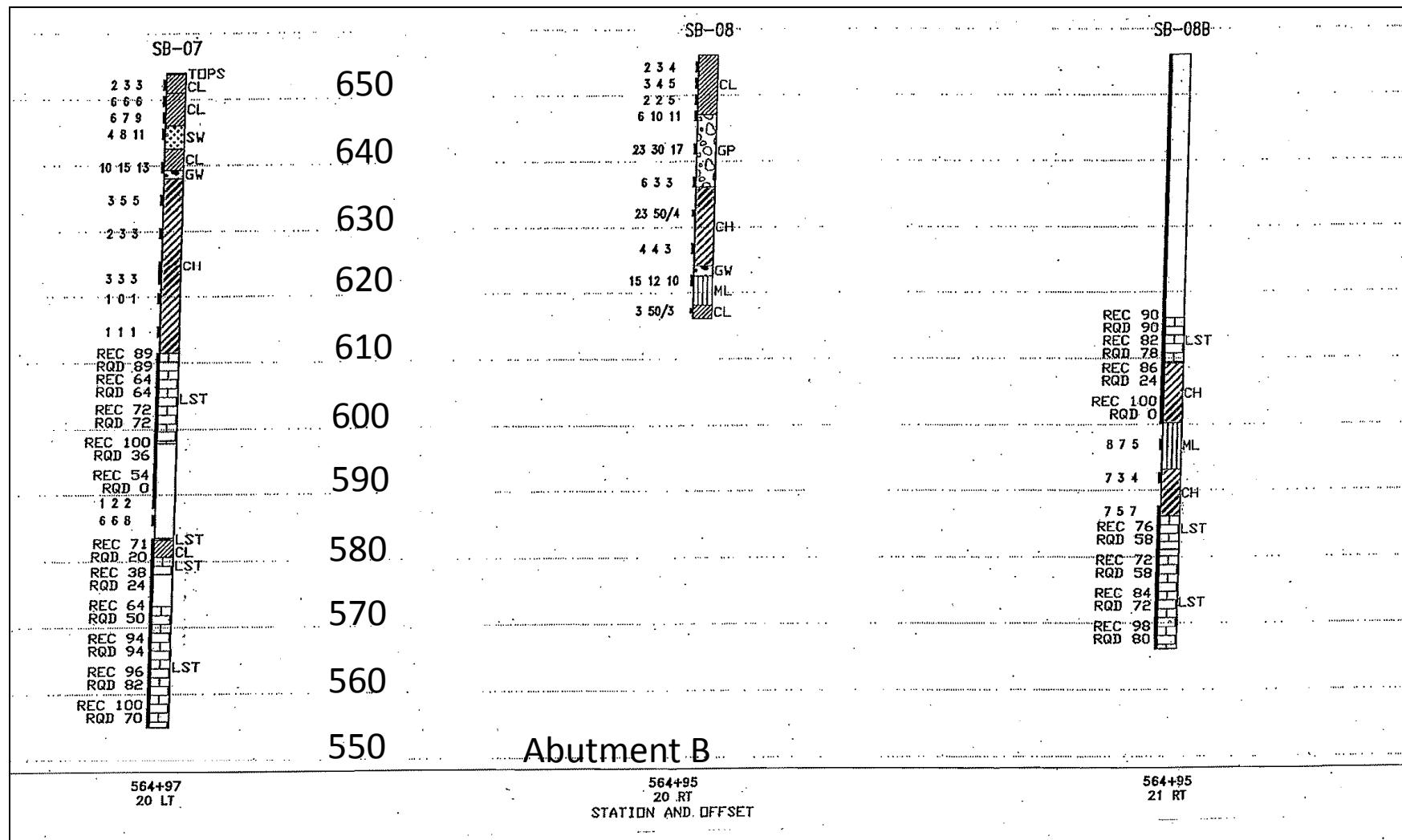
# Boring Logs – Abutment A



# Boring Logs – Pier 2



# Boring Logs – Abutment B



# Foundation Type Selection Considerations

- Variable Conditions (i.e.; erratic and intermittent quality of rock; soil layers and infilling; possible voids)
- Verification of Support Conditions;
- Design for Axial Loads;
- Design for Lateral Loads;
- Settlement and Possible NSF at Abutment Fills

Driven Piles, Drilled Shafts and Micropiles Considered

- Micropiles Selected

# Possible Applications of Micropiles

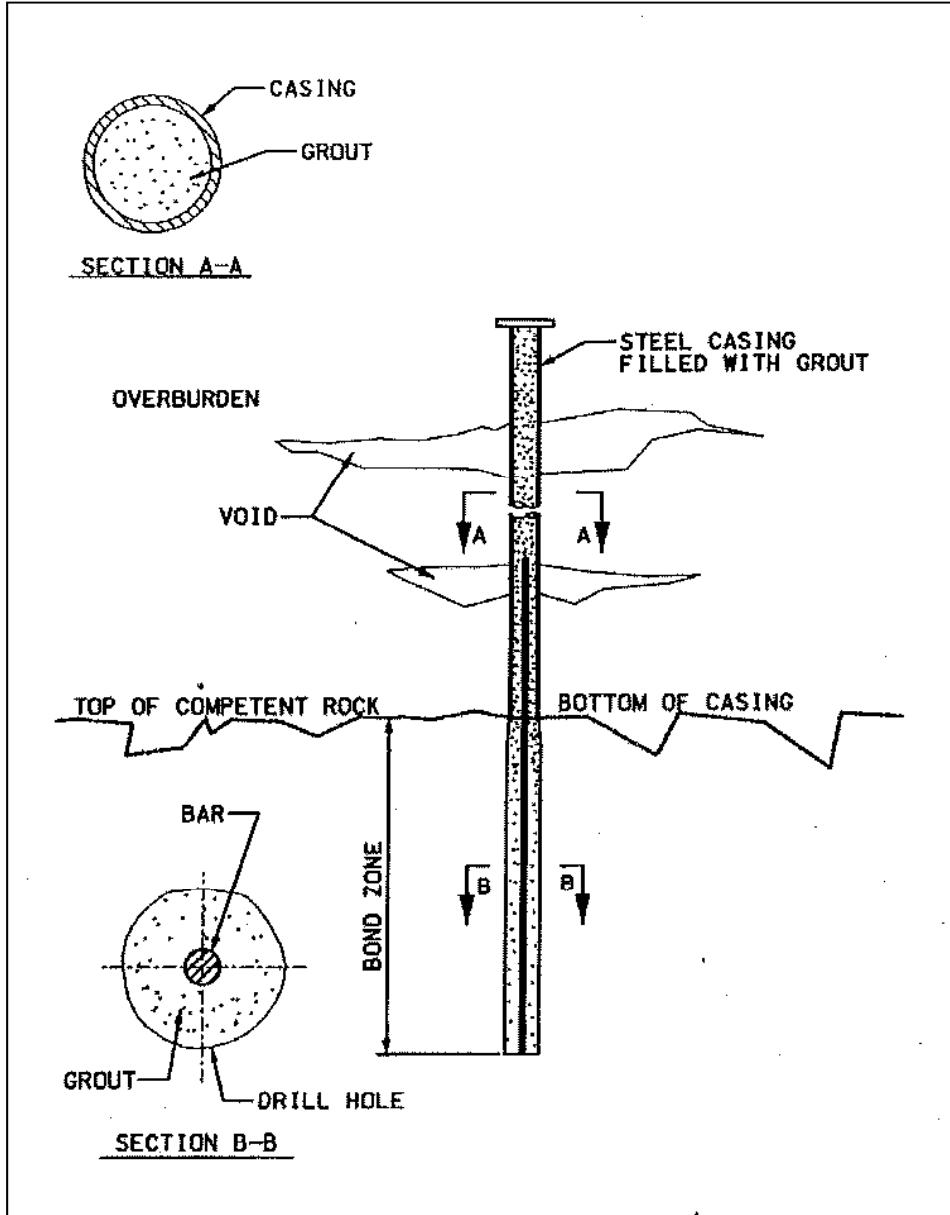
- Restricted Access/Headroom or A Remote Area;
- Support System Close to Existing Structure;
- Supplemental Support For An Existing Structure (e.g. Settlement Control);
- **Difficult Ground Conditions (e.g., karst, mines, boulders, uncontrolled fill);**
- Risk of Liquefaction From Pile Driving;
- Need To Minimize Vibration And/Or Noise;
- Need To Reduce Or Eliminate Spoil At Hazardous Or Contaminated Sites
- As Alternate Deep Foundation Type, Especially Where Piles Penetrate Rock;
- Where Spread Footings Are Feasible but There Is Potential For Erosion or Scour



Ref: FHWA-NHI-05-039

# Micropiles in Karst

- FHWA-NHI-05-039 (Dec,2005)  
“Micropile Design and Construction”
- AASHTO LRFD Bridge Design  
Specifications 4<sup>th</sup> Edition, 2007,  
2008 Interim Section 10.9;
- Other Experiences and Published  
Resources



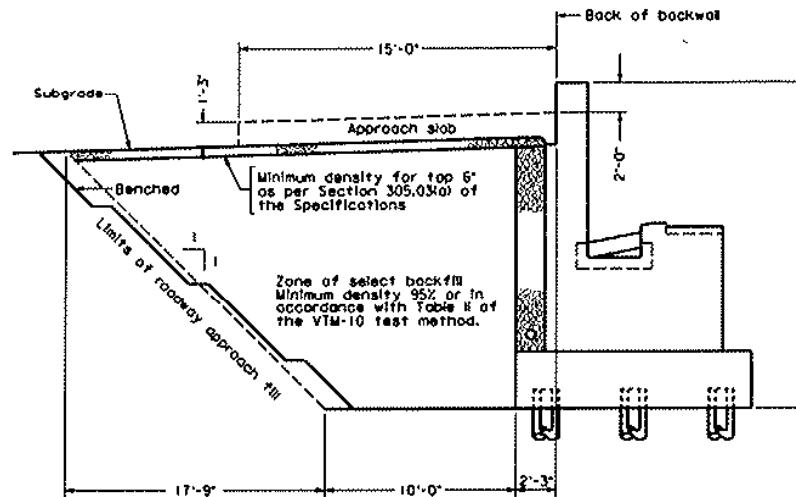
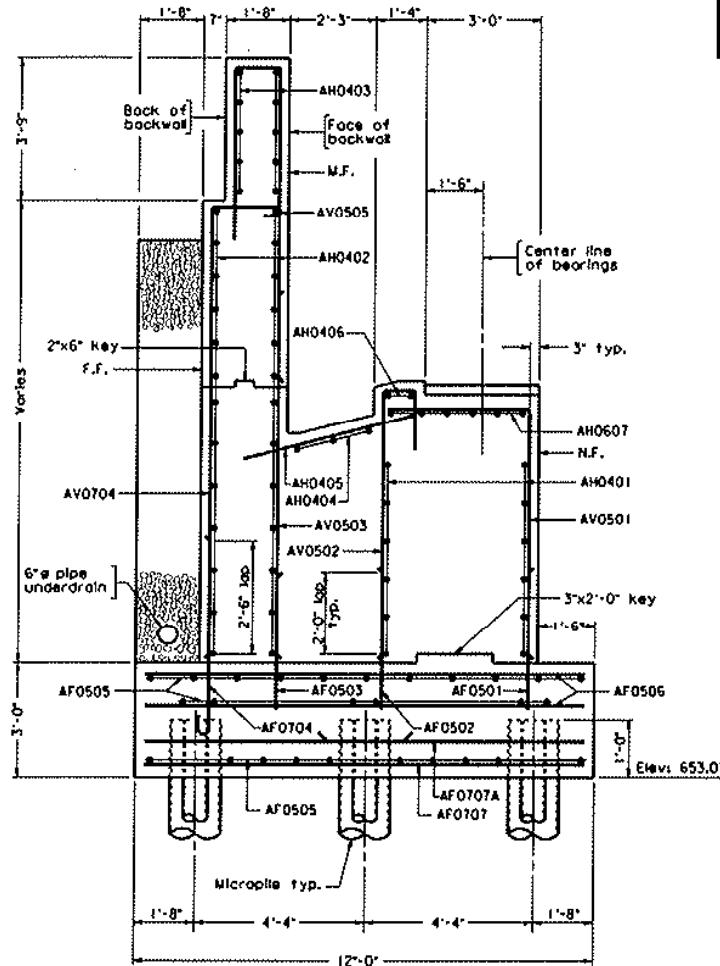
## Micropile Construction in Karst Terrain

- Drill cased hole through soil, boulders and voids;
- Drill through full bond zone to verify conditions;
- No open hole drilling – Drill casing through bond zone;
  - (Use rotary percussive, eccentric duplex method)
- Monitor drilling rates and use to verify bond zone;
- Water testing and seal grouting.
  - (in highly broken/fractured rock or voided karstic rock)

# Design and Construction Considerations

- Bond Zone Design (Nominal & Factored Resistance)
- Provide Preliminary Micropile Design
- Structural Design of Micropiles
- Design for NSF Loads at Abutments
- Design for Possible Void (20' Unsupported Length)
- Specifications for Construction
  - Experience of Specialty Contractor and Personnel
  - Drilling Methods
  - Allow Alternate Designs
  - Installation Plan including MP Documentation
  - Load Testing (Verification and Proof Load Tests)

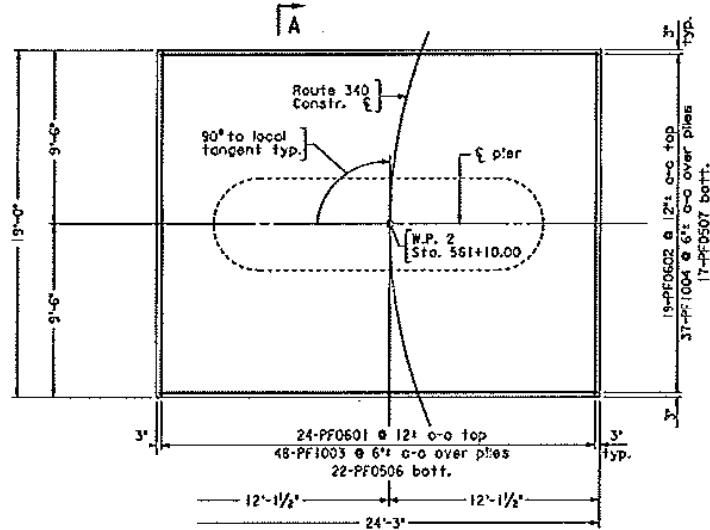
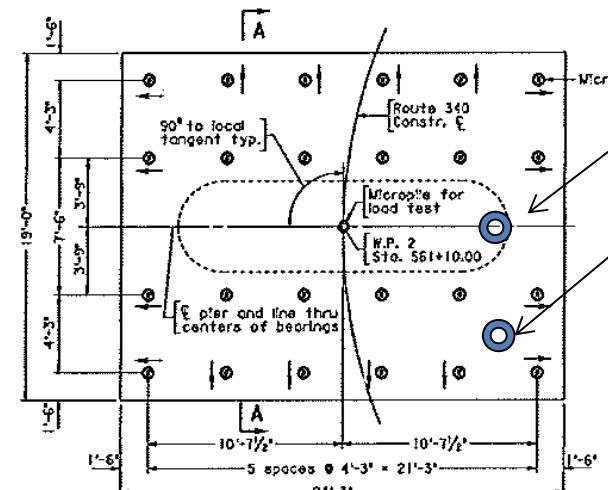
# Micropiles at Abutments



## STRUCTURAL BACKFILL DETAIL

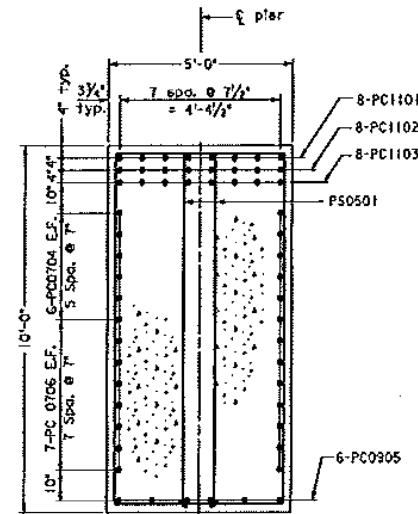
(Dimension measured at Rte. 340 Constr. E)  
Abutment drainage not shown  
Not to scale

## Micropile Grouted Inside Vertical 16-inch OD Casings for Lateral Load Design



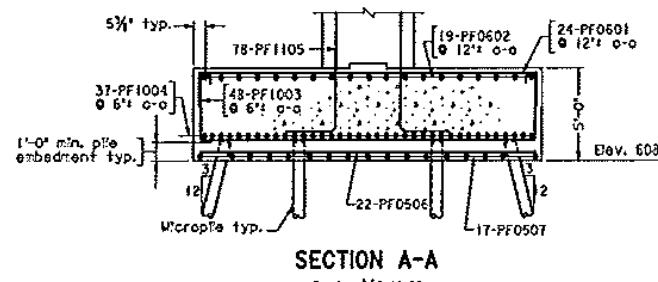
Micropiles not shown for clarity

## Alternate Micropile Positions, If Needed



**SECTION B-B**  
Scale:  $\frac{1}{2} = 1'-0''$

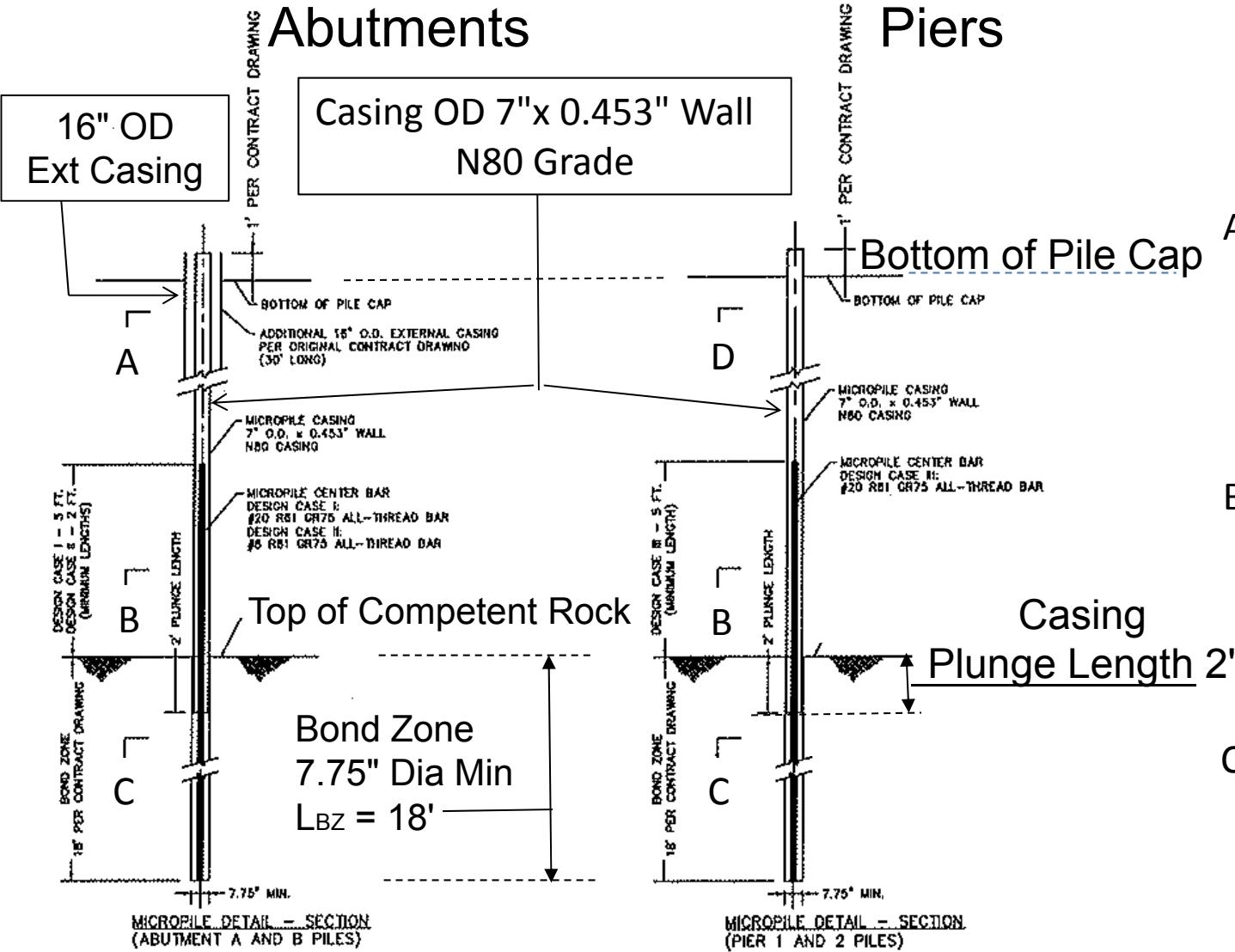
## Micropiles at Piers



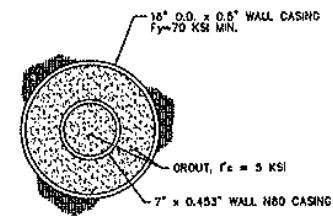
# Abutments

**16" OD  
Ext Casing**

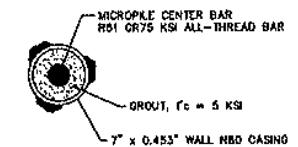
# Casing OD 7"x 0.453" Wall N80 Grade



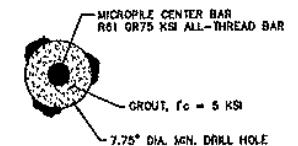
Piers



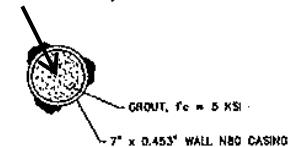
MICROPILE CROSS-SECTION A



MICROPILE CROSS-SECTION B



MICROPILE CROSS-SECTION C



MICROPILE CROSS-SECTION D

# Alternate Micropile Design

# Micropile Axial Load Design (LRFD)

| Foundation            | Design Case | Factored Design Load | Nominal Resistance |
|-----------------------|-------------|----------------------|--------------------|
| Compression           |             |                      |                    |
| Abutments             | I           | 295k                 | 536k               |
|                       | II          | 170k                 | 309k               |
| Piers                 | III         | 392k                 | 713k               |
| Tension Load – 0 kips |             |                      |                    |

Grout-to-Ground  $\alpha_{\text{Bond}}$ , Nominal Resistance = 19.2ksf [135psi]

Resistance Factor (RF) = 0.55

Design Case - Refers to Pile Locations in Foundation

# Micropile Installation and Testing



# Numa T-150 Eccentric Percussive Drill Bit



OD Casing = 7.000"

ID Casing = 6.094"

D Retracted Bit = 5.905"

D Expanded Bit = 7.750"

D Hole min = 7.750"



## Pier 2 MP Installation



# Communication During Drilling



12/19/2011 22:21



12/19/2011 22:04

# Example Micropile Log

Abutment B - Pile 14  
 •Drilling  
 •Initial Grouting

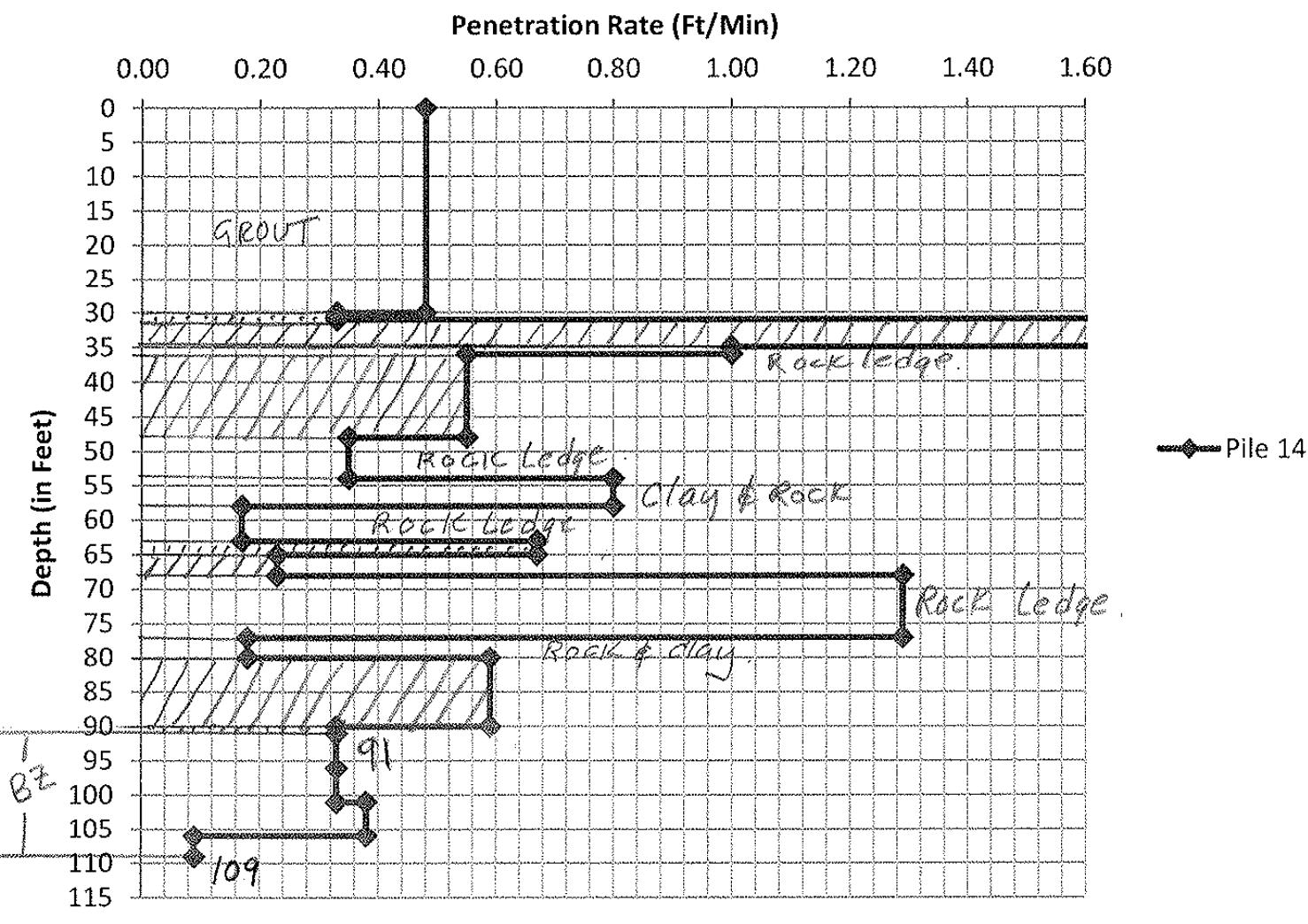
| DATE DRILLED:                                  | 10/13/2011              | DRILLER:                   | G.B.   |       |
|--|-------------------------|----------------------------|--------|-------|
| PROJECT #:                                     | 11-0203                 | TIME START:                | 8:20   |       |
| HOLE #:  | Abut. B - #14           | TIME STOP:                 | 12:32  |       |
| DRILL RIG:                                     | M9-1                    | PILE LENGTH (FROM CUTOFF): | 91.00  |       |
| HOLE DIA.:                                     | 7.75"                   | DRILL EL.:                 | 662.33 |       |
|  |                         | TIP EL:                    | 553.33 |       |
|  |                         |                            |        |       |
| SOIL / ROCK DESCRIPTION                        | COMMENTS / DIFFICULTIES | TIME                       | FROM   | TO    |
| Grout  |                         | 8:20                       | 0.0    | 30.0  |
| Broken Rock                                    |                         | 9:22                       | 30.0   | 31.0  |
| Clay   |                         | 9:25                       | 31.0   | 35.0  |
| Rock Ledge                                     |                         | 9:27                       | 35.0   | 36.0  |
| Clay   |                         | 9:28                       | 36.0   | 48.0  |
| Rock Ledge                                     |                         | 9:50                       | 48.0   | 54.0  |
| Clay/Rock                                      |                         | 10:07                      | 54.0   | 58.0  |
| Rock Ledge                                     |                         | 10:12                      | 58.0   | 63.0  |
| Broken Rock                                    |                         | 10:42                      | 62.0   | 65.0  |
| Clay   |                         | 10:45                      | 65.0   | 68.0  |
| Rock Ledge                                     |                         | 10:58                      | 68.0   | 77.0  |
| Rock/Clay                                      |                         | 11:05                      | 77.0   | 80.0  |
| Clay   | Soft                    | 11:22                      | 80.0   | 90.0  |
| Broken Rock                                    |                         | 11:39                      | 90.0   | 91.0  |
| Rock   |                         | 11:42                      | 91.0   | 96.0  |
| Rock   |                         | 11:57                      | 96.0   | 101.0 |
| Rock   |                         | 12:12                      | 101.0  | 106.0 |
| Rock   |                         | 12:25                      | 106.0  | 109.0 |
| <i>Rock Socket Time Start:</i>                 |                         | 11:42                      |        |       |
| <i>Rock Socket Time Stop:</i>                  |                         | 12:32                      |        |       |
| GROUTING INFORMATION                           |                         | MATERIALS USED / COMMENTS  |        |       |
| DATE GROUTED:                                  | 10/13/2011              | CASING USED:               | 93'    |       |
| GROUT TAKE:                                    | 461.3 gallons           | CENTRAL REINFORCEMENT:     |        |       |
| GROUT COMMENTS                                 |                         | GENERAL COMMENTS           |        |       |
| This hole would not grout up. Needs redrilled. |                         |                            |        |       |

# Example Micropile Log

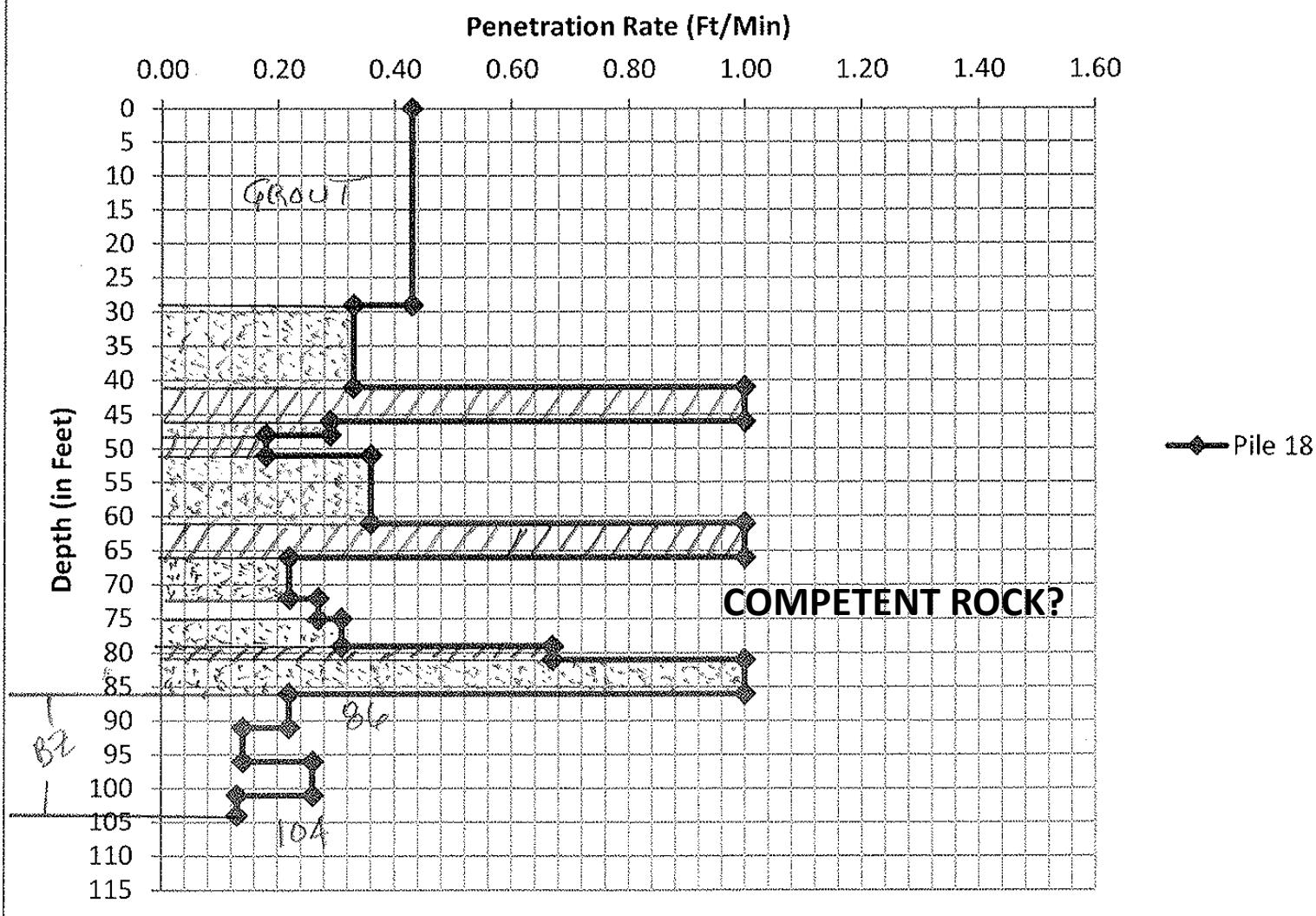
## Abutment B - Pile 14

- Re-Drilling
- Re-Grouting

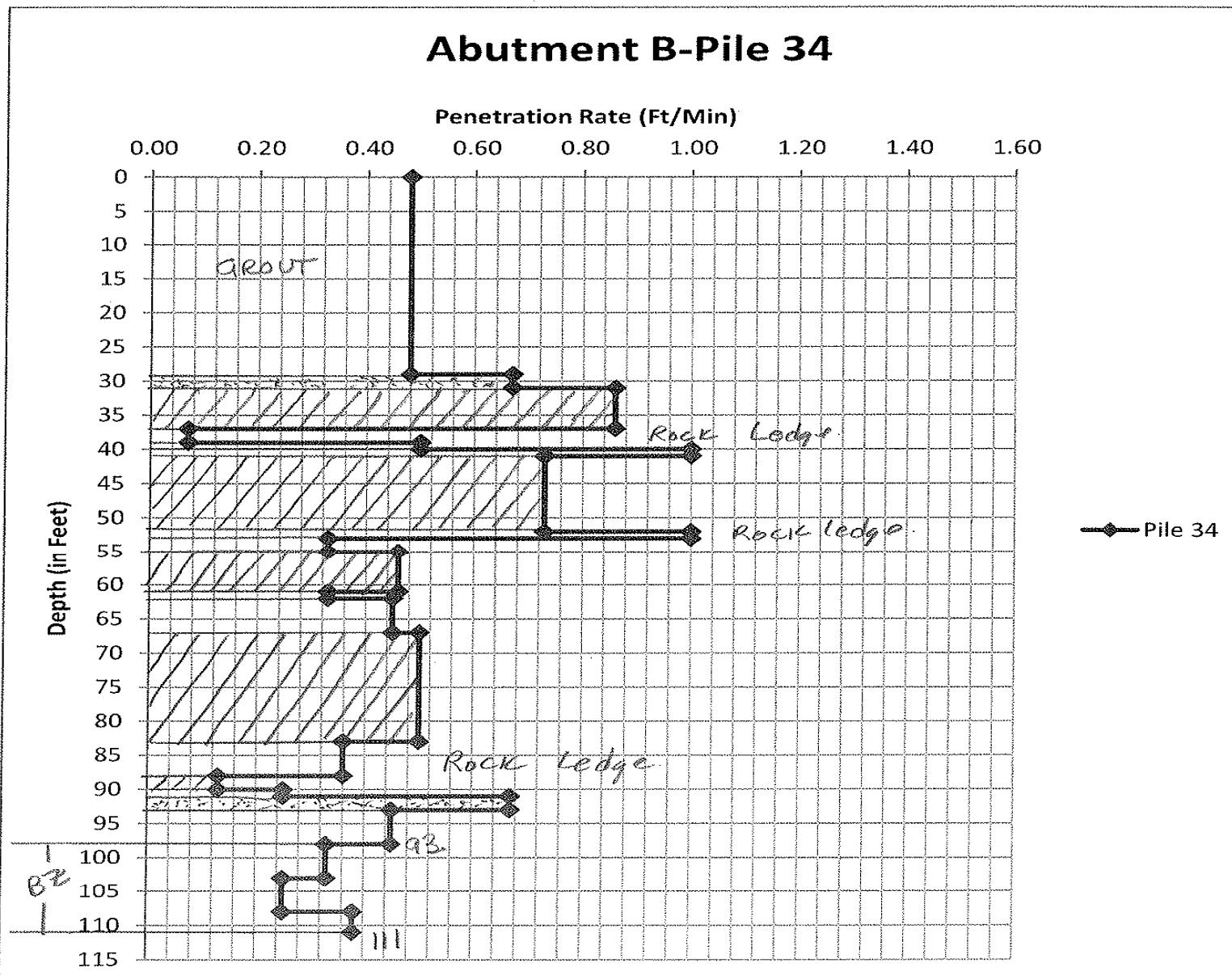
## Abutment B-Pile 14



## Abutment B-Pile 18



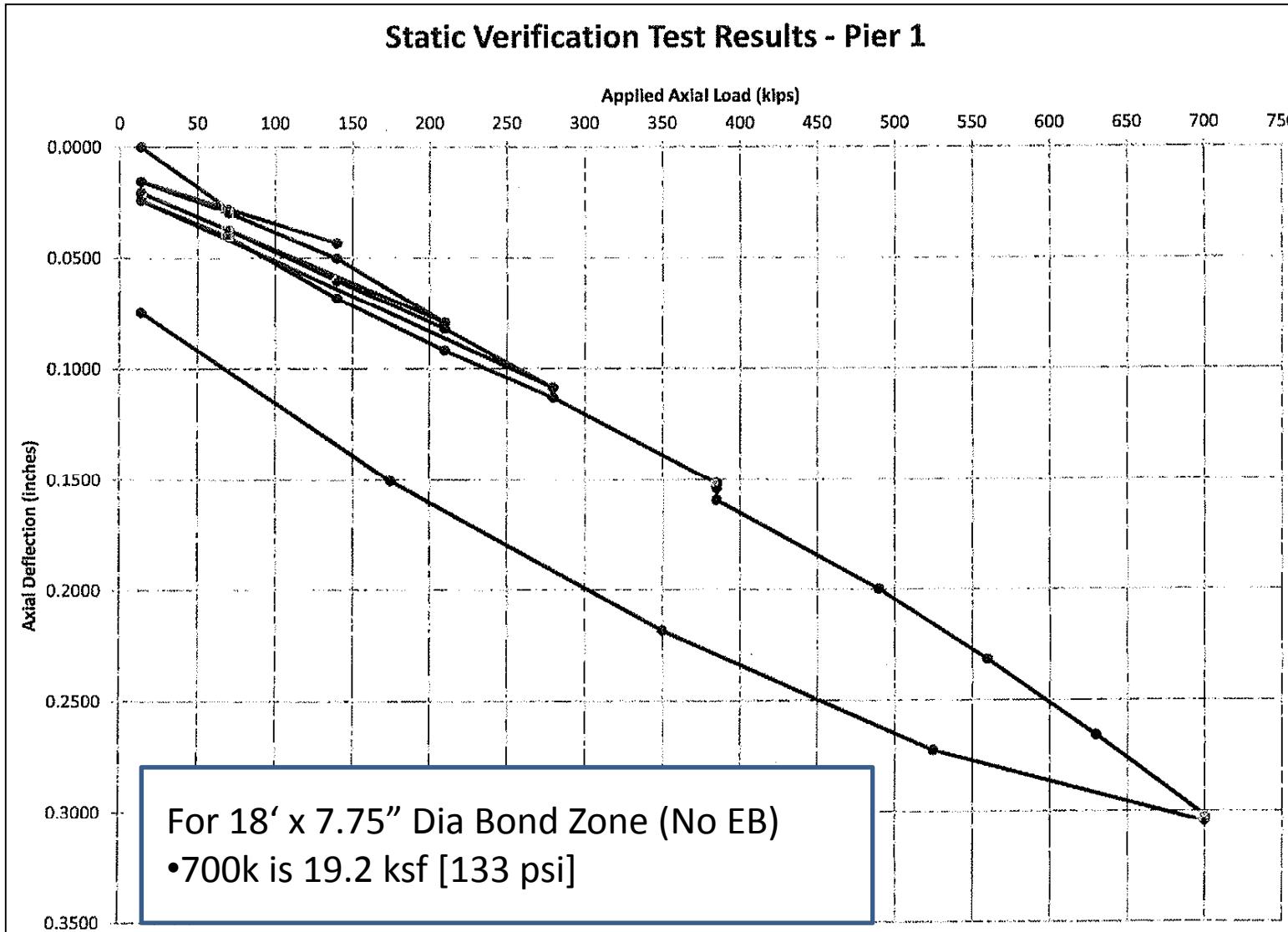
## Abutment B-Pile 34



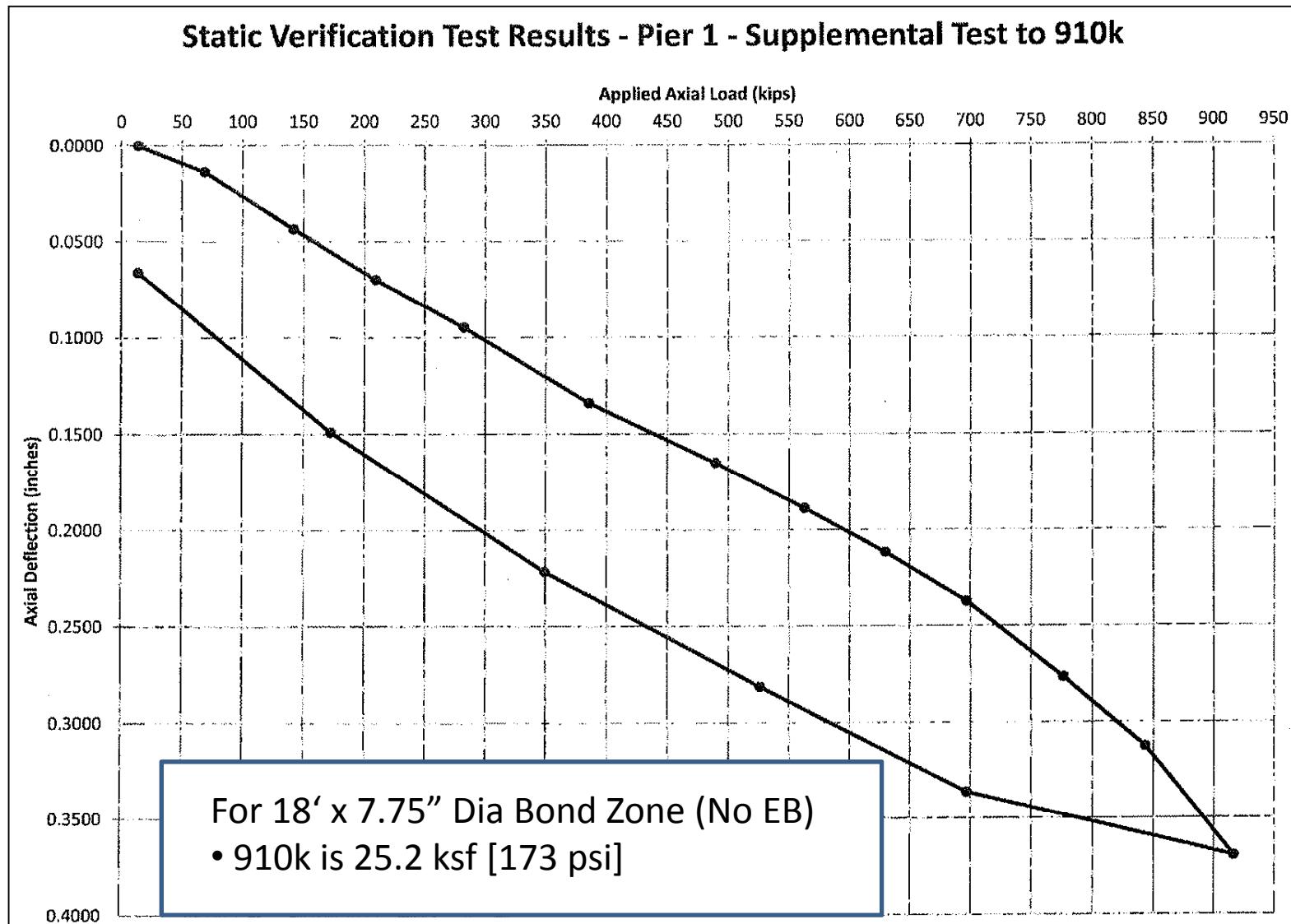
## Load Testing Arrangement



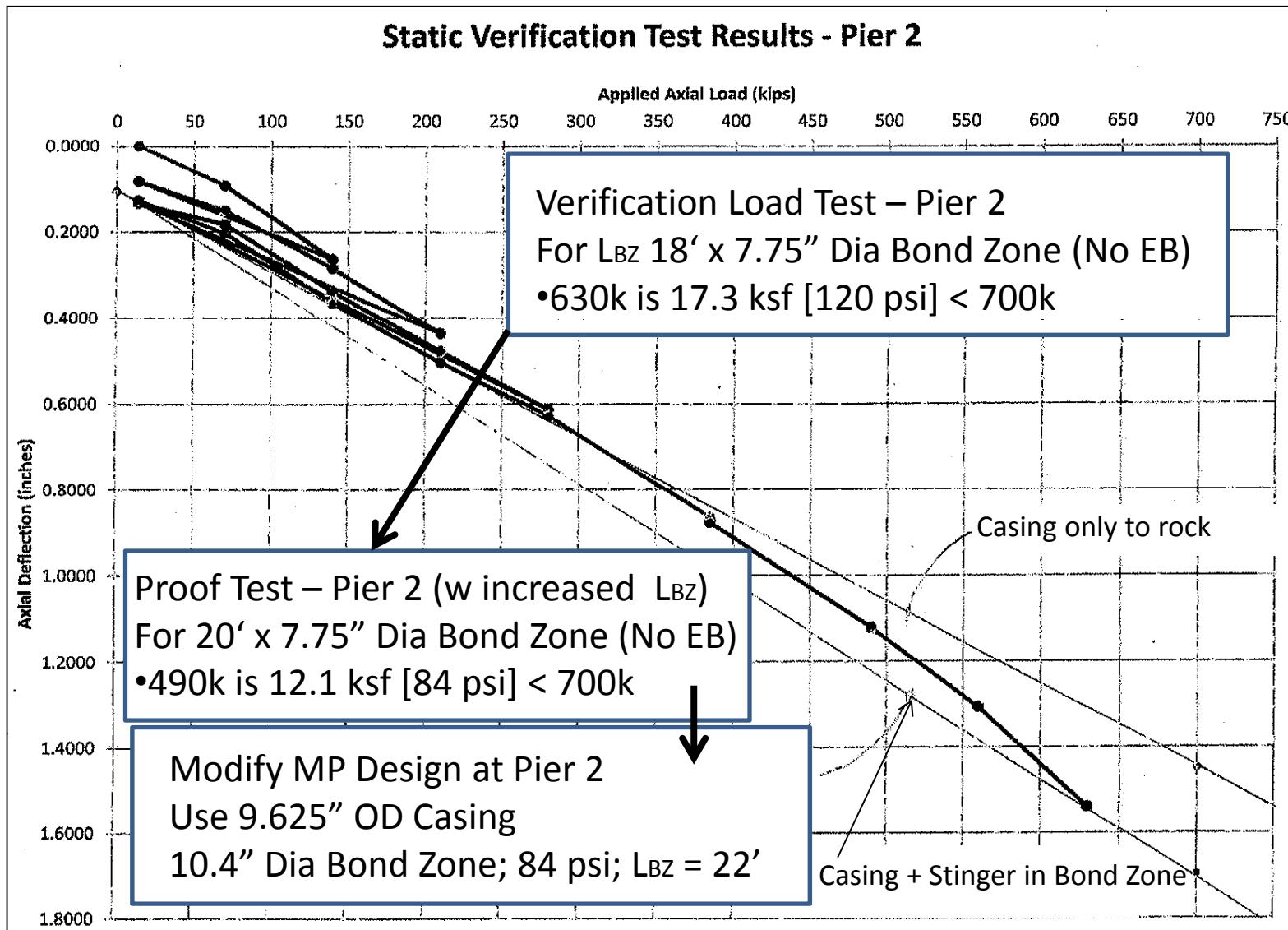
# Verification Load Test – Pier 1



# Verification Load Test (Supplemental) – Pier 1

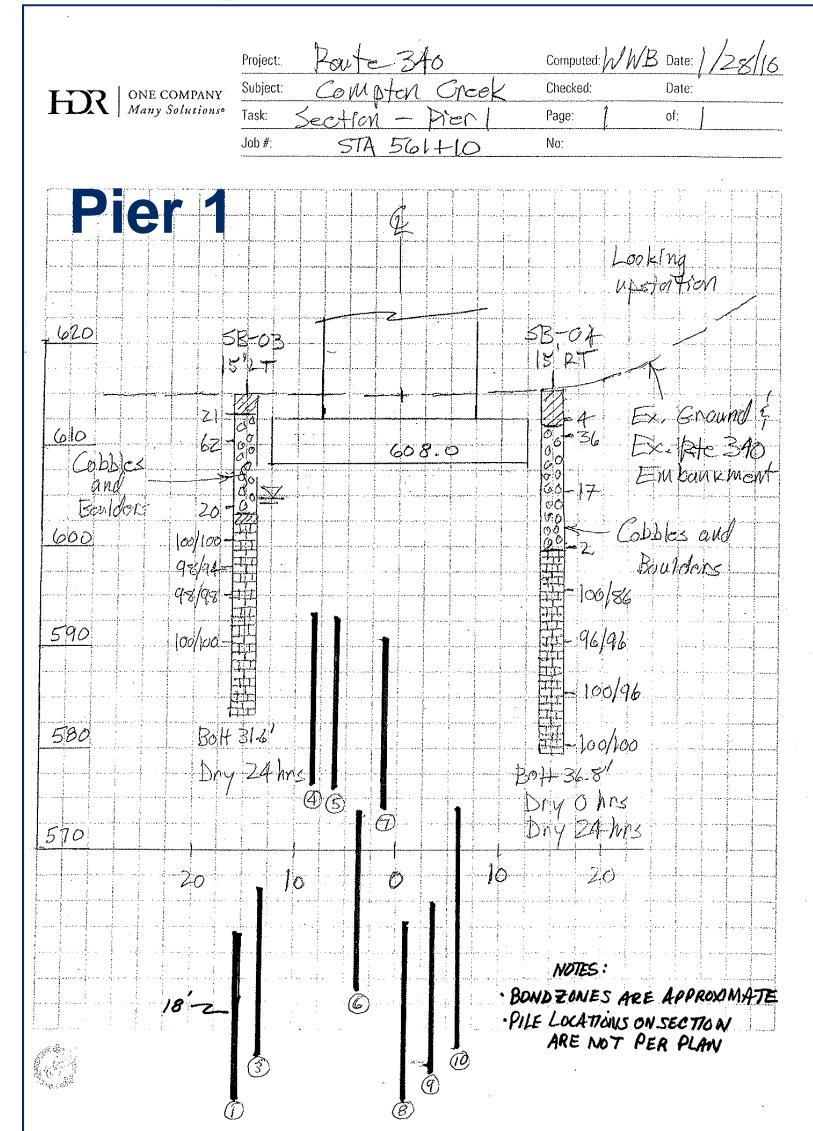
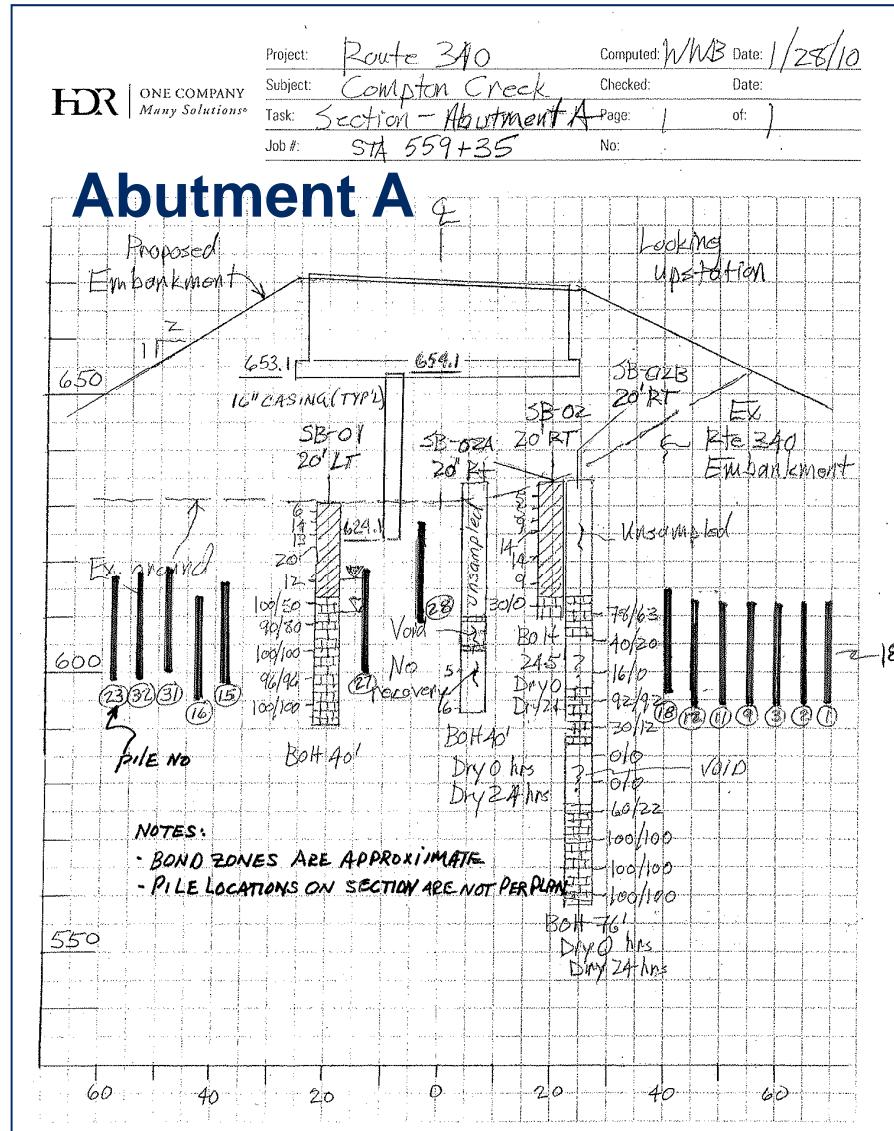


# Verification Load Test – Pier 2

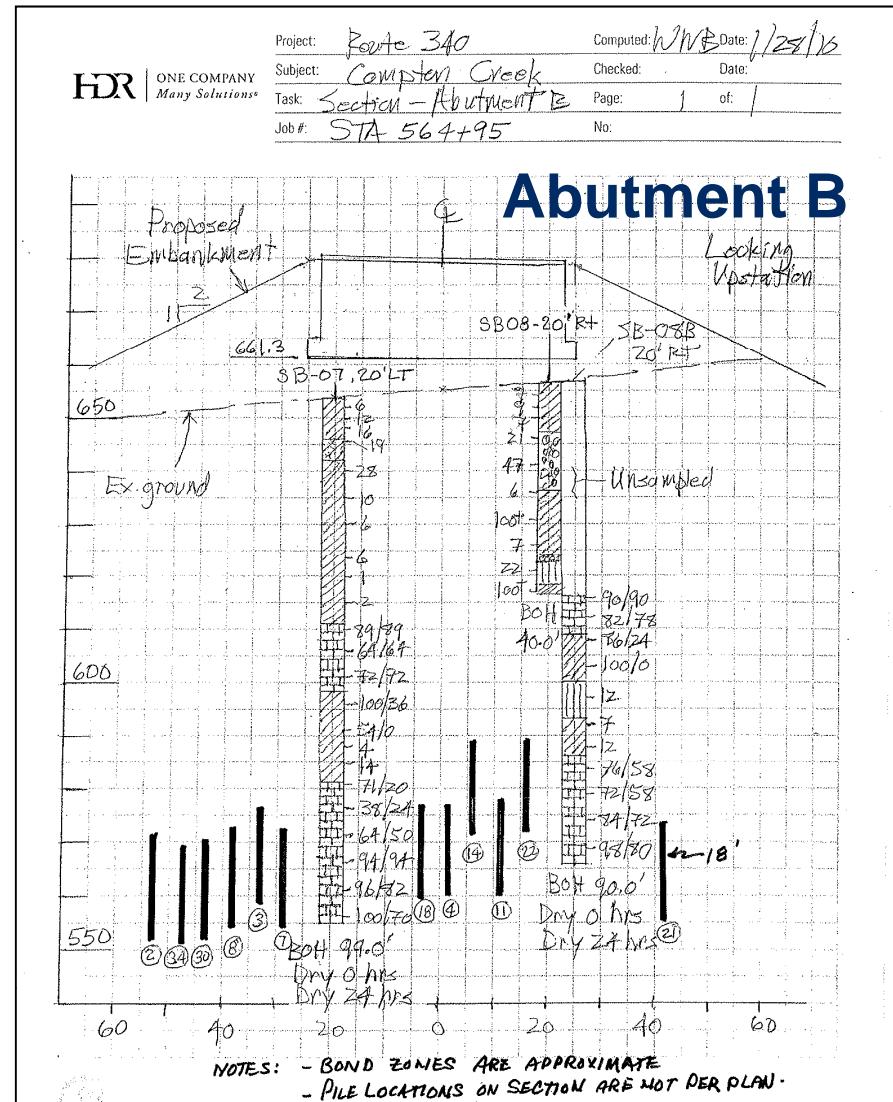
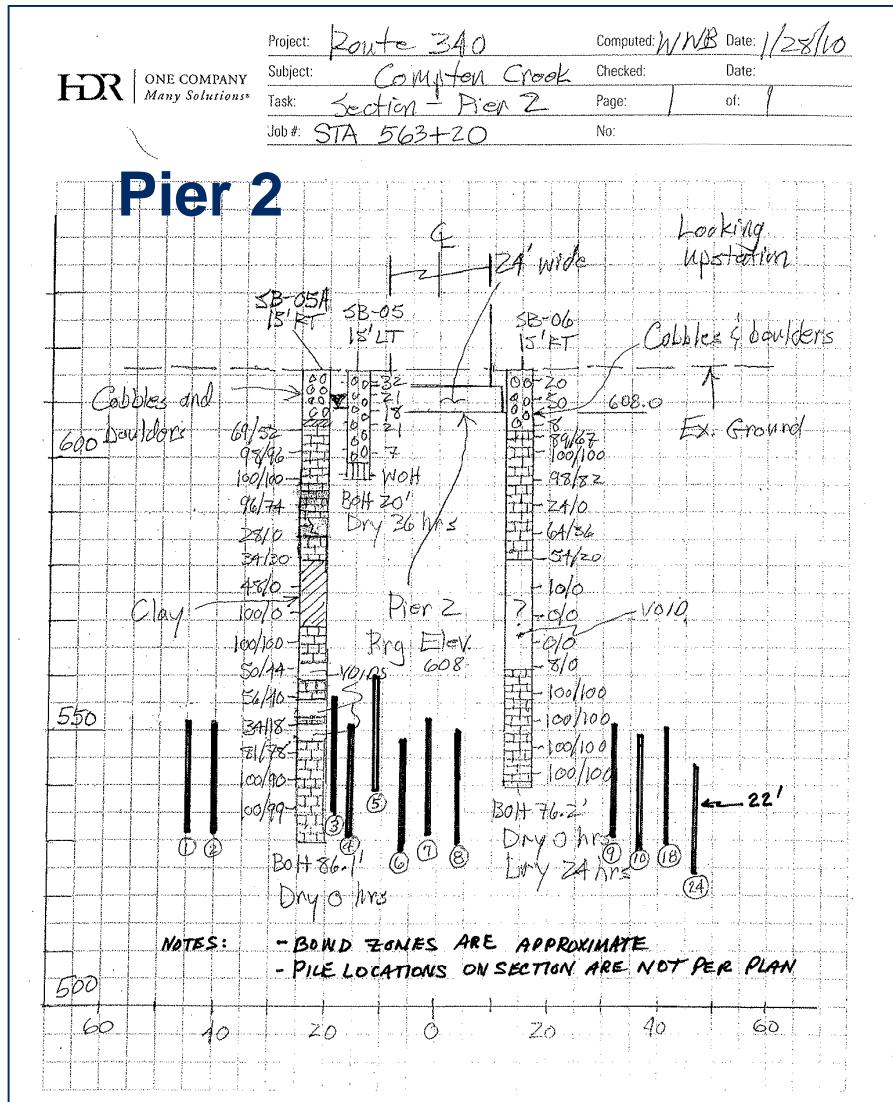


Increase bond zone length 10%...get a 20% reduction in capacity!

# Schematic Sections with Micropile Bond Zones



# Schematic Sections with Micropile Bond Zones



# Alternate Load Testing Methods

## [Review for Limitations]

### GRL's Apple



### Birminghamner – AFT Statnamic





2012 6 13

View from Abutment A – looking north.

2012 STGEC



2012 6 13

View south, Pier 2, with Pier 1 in background.

## Concluding Comments

- Design and construction in karst geology is uniquely challenging.
- Micropiles are a feasible deep foundation support elements in karst.
- Care must be taken to sufficiently characterize subsurface conditions during design and confirm during construction.
- Contract documents need to be developed to capture the design intent without being overly restrictive; karst demands the ability to adapt to erratic and varying conditions.
- Experience is essential.

Thank You  
Questions?